SYNTHESIS OF NON UNIFORM LINEAR ARRAYS USING DOLPH – CHEBYSHEV POLYNOMIAL BY REDUCING SIDE LOBE LEVEL BASED ON MODULATING PARAMETER ARRAY FACTOR

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ABSTRACT

In this paper a new approach to reduce the first side lobe level of an antenna array, without disturbing the main beam width using dolph – chebyshev array. There are number of Techniques used to reduce Side Lobe Level (SLL) of antenna arrays to save power and improve Quality of Service (QoS) by ensuring maximum radiation in desired direction, several methods are available in literature. However, in the present work, an array for a specified first side lobe level of -35dB was synthesized using Dolph Chebyshev method. The weighting vectors are compared. Using these vectors, patterns are generated for arrays of different elements. The resultant patterns are compared and the result shows greater improvement in the SLL reduction from the Dolph Chebyshev method without deteriorating the main beam width.

Keywords: Non uniform antenna arrays, Array Factor, dolph - Chebyshev , side lobe level, beam width.

I. INTRODUCTION

Usuall the radiation pattern of a single element is relatively wide and each element provides low values of directivity. Antenna arrays increase the directivity without enlarging the size of single elements. Antennas arrays have been widely used in different applications are radar, sonar, and communications and as they are useful in high power transmission, reduce power consumption and enhanced spectral efficiency. Due to increased usage of electromagnetic spectrum, radiation pattern synthesis techniques, which allow placing of one or more nulls in the pattern in specified directions, are gaining technical importance. Array antenna have high gain and directivity compared to an individual radiating element.

In most of the applications, side lobes are generally unwanted and the first side lobe level usually introduces Electromagnetic Interference (EMI) problems and hence it should be lowered without disturbing the beam width. Side lobe level (SLL) reduction has a great importance in recent communication systems. It is considered as one of the most important applications of digital beam forming since it reduces the effect of interference arriving outside the main lobe.
when the first side lobe is reduced, null to null beam width is increases. This leads to great disturbance in the
directivity of the array. In this paper, one method is used for the synthesis of the antenna array. That is Dolph
Chebyshev. With Dolph Chebyshev method, the excitation coefficients are obtained and the patterns are
presented for different arrays. In order to reduce the first side lobe level and without disturbing the main beam
width.

II. RELATED WORK

Antenna is a metallic device which acts as transducer. It converts electrical waves to electromagnetic waves
while transmitting and vice versa while receiving. An antenna array is a group of identical antenna elements
arranged usually in a regular fashion. In a linear array, the elements are arranged along a straight line and are
often fed coherently. The currents through the elements are generally different in amplitudes and phases in order
to obtain greater control over the radiation pattern. Basically the antenna array design involves calculating the
complex currents of the individual antenna elements and selecting an appropriate antenna element. The current
excitations would largely determine how sharp the resultant radiation pattern is and how small the side lobe
levels are in comparison to the main lobe. In antenna design, it is required to obtain narrowest main beam width
along with low side lobe levels. It was found that as the current amplitude taper from the center to the edges of
the array increased, the side-lobe level decreased, but with an increase in the width of the main beam. In most
applications, it is desirable to have both a narrow main beam as well as low side lobes. It would, therefore be
useful to have a pattern with an optimum compromise between beam width and side-lobe level.

III. PROPOSED METHOD

We propose a Dolph – chebyshev array method to synthesize the array beam pattern of a Non Uniform Linear
Array (NULA) based on the properties of Chebyshev polynomials. For a given Side-Lobe Level (SLL), it has
been proven that the Dolph-Chebyshev array provides narrowest main beam width in the array beam pattern,
while for a given main beam width, it achieves the lowest SLL.

Fig 1: Functional Block Diagram of Dolph - Chebyshev Array

Dolph proposed (in 1946) a method to design arrays with any desired side-lobe levels and any HPBWs. This
method is based on the approximation of the pattern of the array by a Chebyshev polynomial of order \( n \), high
enough to meet the requirement for the side-lobe levels. A DCA with no side lobes (side-lobe level of \(-\infty\) dB)
reduces to the binomial design. The trade-off between the side-lobe levels (SLL) and the half-power beam width (HPBW) stimulate the question answered primarily by Dolph of obtaining the narrowest possible beam width for a given side-lobe level or the smallest side-lobe level for a given beam width. This was possible by using the orthogonal functions of Chebyshev in order to design an optimum radiation pattern. However, for large number of elements this procedure becomes quite cumbersome since it requires matching the array factor expression with an appropriate Chebyshev function. To over-come this deficiency, proposed a new formulation for the design of Chebyshev arrays based on solving a system of linear equations. Iterative procedure was used to produce the desired pattern.

The Chebyshev polynomials:

\[ T_n(x) = \begin{cases} 
(-1)^n \cosh(n \cosh^{-1}|x|) & x < -1 \\
\cos(n \cos^{-1} x) & -1 < x < 1 \\
\cosh(n \cosh^{-1} x) & x > 1
\end{cases} \]

\[ T_0(x) = 1 \]

\[ T_1(x) = x \]

\[ T_2(x) = 2x^2 - 1 \]

\[ T_3(x) = 4x^3 - 3x \]

\[ T_4(x) = 8x^4 - 8x^2 + 1 \]

... 

\[ T_{n+1}(x) = 2xT_n(x) - T_{n-1}(x) \]

\[ n = 0 \cos(nu) = 1 = T_0(z) \]

\[ n = 1 \cos(nu) = z = T_1(z) \]

\[ n = 2 \cos(nu) = 2z^2 - 1 = T_2(z) \]

\[ n = 3 \cos(nu) = 4z^3 - 3z = T_3(z) \]

\[ n = 4 \cos(nu) = 8z^4 - 8z^2 + 1 = T_4(z) \]

\[ n = 5 \cos(nu) = 16z^5 - 20z^3 + 5z = T_5(z) \]

\[ n = 6 \cos(nu) = 32z^6 - 48z^4 + 18z^2 - 1 = T_6(z) \]

\[ n = 7 \cos(nu) = 64z^7 - 112z^5 + 56z^3 - 7z = T_7(z) \]

\[ n = 8 \cos(nu) = 128z^8 - 256z^6 + 160z^4 - 32z^2 + 1 = T_8(z) \]

\[ n = 9 \cos(nu) = 256z^9 - 576z^7 + 432z^5 - 120z^3 + 9z = T_9(z) \]
Fig 2: Chebyshev Polynomials $T_0(x), T_1(x), T_2(x), T_3(x)$ and $T_4(x)$

A criterion that can be used to judge the relative beam width and side lobe level of one design to another is the amplitude distribution (tapering) along the source. It has been shown analytically that for a given side lobe level the Dolph-chebyshev array produces the smallest beam width between the first nulls. Conversely, for a given beam width between the first nulls, the Dolph-chebyshev design leads to the smallest possible side lobe level. Chebyshev polynomials such as lower far outside-lobes and higher beam efficiency.

3.1 Design Equations

If elements of the array are placed along a line then such a configuration is termed as linear antenna array. The geometry is as shown in fig.3. In synthesis of linear antenna arrays the elements are considered to be isotropic radiators.

3.2 Array Factor

The array factor is a function of the geometry of the array and the excitation phase. By varying the separation $d$ and/or the phase $\beta$ between the elements, the characteristics of the array factor and of the total field of the array can be controlled.

$$AF = 2 \sum_{n=1}^{N} I_n \cos\left[\frac{2n-1}{2}kd \sin(\theta) + \phi_n\right]$$
Where

- \( \theta \) - Zenith angle
- \( I_n \) - Current excitation amplitude
- \( \psi_n \) – Phase of the nth array element
- \( d \) - The inter element spacing between the radiating element
- \( k \) - Wave number of the carrier signal is \( k=2\pi/\lambda \).

**Fig 4:** Array Factor for a 5 Element ULA with a Spacing of 0.5 m

### 3.3 Fitness Function

The Fitness Function is from the Array Factor in such that the objective of the optimization is satisfied. The general form of the fitness function is given by

\[
FF = \sum_{\theta=-90^\circ}^{90^\circ} W(\theta)[F_0(\theta) - F_d(\theta)]
\]

Where

- \( F_0(\theta) \) – The pattern obtained using the proposed algorithm.
- \( F_d(\theta) \) – The desired pattern.
- \( W(\theta) \) - The weight vector to control the side lobe level in the cost function.

### IV. SIMULATION RESULTS

**Fig 5.1:** Optimized Radiation pattern with reduced side lobe level for N=8 elements array for Broad side array

**Fig 5.2 :** Optimized Radiation pattern with reduced side lobe level for N=8 elements array for Dolph–chebyshev array
Fig 5.3: Optimized Radiation pattern with reduced side lobe level for N=15 elements array for Broad side array

Fig 5.4: Optimized Radiation pattern with reduced side lobe level for N=15 elements array for Dolph–chebyshev array

Fig 5.5: Polar plot of Broad side array for N=8

Fig 5.6: Polar plot of Dolph–chebyshev array for N=8

Fig 5.7: Polar plot of Broad side array for N=1

Fig 5.8: Polar plot of Dolph–chebyshev array for N=15
Table 1: Compression of Antenna Arrays

<table>
<thead>
<tr>
<th>INPUT</th>
<th>OUTPUT</th>
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<tbody>
<tr>
<td>Type of Array</td>
<td>Number of elements</td>
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<td>Broad side array</td>
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<tr>
<td></td>
<td>15</td>
</tr>
<tr>
<td>End fire array</td>
<td>8</td>
</tr>
<tr>
<td></td>
<td>15</td>
</tr>
<tr>
<td>Dolph–chebyshev array</td>
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<td>15</td>
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V. CONCLUSION

This research work proved the power of using Dolph–chebyshev array in solving complex problems where you have conflicting constrains. The first side lobe level which introduces Electromagnetic Interference (EMI) problems is lowered without disturbing the main beam width. The parameters obtained by applying dolph–chebyshev array. For 15 element array SLL = –40 dB, HPBW = 9.6°. Dolph–chebyshev array finds the beam width and side lobe level with N=8, 15. It can be seen that the current excitation values obtained from the dolph–chebyshev for all the number of elements simulated compare to other arrays, while at the same time, the first null–to–null beam width is slightly reduced as well as reduces the side lobe levels.

REFERENCES


**AUTHORS BIOGRAPHY**

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