



Experimental Investigation on Dissimilar Welding of

Austenite and Ferrite Stainless Steel

by MIG Welding Process

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ABSTRACT

Joining of dissimilar metals is really a challenging task due to difference in their thermal, mechanical and chemical properties welded under a common welding condition. A variety of problems evolves in dissimilar welding like cracking, large weld residual stress, migration of atoms during welding causing stress concentration on one side of the weld, compressive and tensile stresses, stress corrosion cracking etc. To overcome these challenges, it is required to study the effect of welding process parameter on mechanical property. However, joining of dissimilar metals has found its use extensively in power generation, electronic, petrochemical and chemical industries, nuclear reactors due to environmental concerns, energy saving, high performance, cost saving and so on.

The aim of this research is to experimentally investigate the dissimilar welding of Austenitic Stainless Steel (AISI 316) and Ferritic Stainless Steel (AISI 430) weld ment using ER 304L by MIG(commonly known as GMAW) welding process. The effects of the various parameters like current and voltage for MDR, heat input, tensile strength, percentage elongation, temperature profile of the weld zone and metallography have been clearly depicted in the respective sections.It has been reported that at low and moderate current MDR, weld width and tensile strength all increase but at high temperature these properties show tremendous decline in their values.

Keywords: Austenite, Ferrite, MIG Welding, GMAW,316-430 Dissimilar Welding

I. INTRODUCTION

Welding is a manufacturing process of creating a permanent joint obtained by the fusion of the surface of the parts dissimilar to each other. The heat required for the fusion of the material may be obtained by burning of gas or by an electric arc. The latter method is more extensively used because of greater welding speed. Welding is extensively used in fabrication as an alternative method for casting or forging and as a replacement for bolted and riveted joints. It is also used as a repair medium e.g. to reunite a metal at a crack or to build up a small part that has broken off such as a gear tooth or to repair a worn surface such as a bearing surface.to be joined together, with or without the application of pressure and a filler material. The materials to be joined may be similar or

II. MATERIAL SELECTION & PROPERTIES

This chapter studies about the types of stainless steels involved in this project such as ferritic stainless steel and austenitic stainless steel and their properties. Stainless Steels are iron-base alloys containing 10% or more chromium, which imparts to the metal the corrosion-resistant properties for which stainless steels are so highly regarded.

2.1. Workpiece material

The materials used to carry out experiment are Austenetic Stainless steel AISI 316 and Ferritic Stainless steel 430. The chemical composition and properties of Stainless steel AISI 316 and 430 are shown in table 2.1 and 2.2 respe.

Table 2.1: Chemical Composition of AISI 316 &430

| SL NO. | ELEMENTS | %WEIGHT (TYPE 316) | %WEIGHT (TYPE 430) |
|--------|-------------|-----------------------|-----------------------|
| 1. | Carbon | 0.08 | 0.12 |
| 2. | Manganese | 1.51 | 1 |
| 3. | Silicon | 2.9 | 1 |
| 4. | Chromium | 17.4 | 16-18 |
| 5. | Phosphorous | 0.04 | 0.04 |
| 6. | Molybdenum | 1.96 | |
| 7. | Nickel | 9.5 | 0.5 |
| 8. | Cobalt | 0.51 | |

Table 2.2: Properties of AISI 316 & AISI 430

| SLNO. | PROPERTY | AISI 316 | AISI 430 |
|-------|-------------------------------|----------|----------|
| 1. | Density in kg/m ³ | 8000 | 7750 |
| 2. | Elastic modulus in MPa | 193 | 200 |
| 3. | Thermal conductivity in W/Kgk | 16.3 | 26.1 |
| 4. | Specific heat in J/Kgk | 500 | 460 |
| 5. | Tensile strength | 515 | 483 |
| 6. | Yield strength in Mpa | 205 | 310 |

2.2 Filler metal

The filler material used for the experiment is Stainless steel ER304 electrodes with size of 1.20 mm diameter

Table 2.3: Composition of ER 304 electrode

| ELEMENTS | COMPOSITION |
|-------------|-------------|
| Carbon | 0.03 |
| Manganese | 2 |
| Phosphorous | 0.045 |
| Sulphur | 0.03 |
| Silicon | 1 |
| Chromium | 18-20 |
| Nickel | 8-12 |

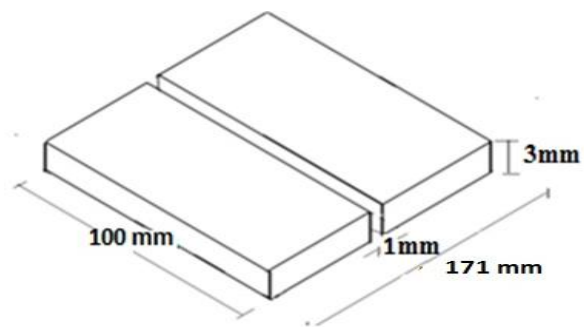


Fig.3.2: Square butt joint for MIG welding

2.3. Shielding Gas

The shielding gas used is CO₂. This gas has been used as it produces the deepest penetration.

III. EXPERIMENTAL WORK AND SAMPLE PREPARATION

3.1. Sample preparation for welding

Table 3.1: Welding condition and process parameters

| Process parameter | Value |
|--------------------------------|------------------|
| Welding current(Amp) | 60,80,90 and 100 |
| Welding speed(mm/sec) | 1.7 |
| Electrode polarity | DCEP |
| Arc voltage(volt) | 20,25 ,30 and 30 |
| Filler wire diameter(mm) | 1.2 |
| Electrode | ER304L |
| Number of passes | 1 |
| Shielding gas flow rate(L/min) | 10 |
| Feed rate(m/min) | 3.2 |
| Stick out length(mm) | 12 |

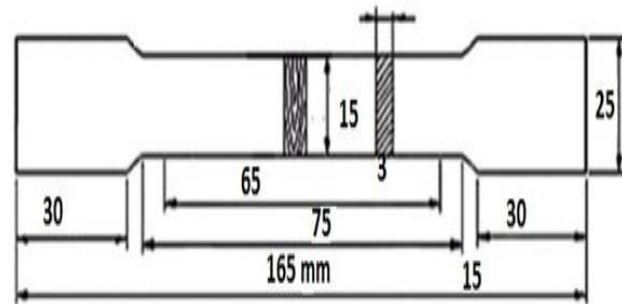


Fig.3.1& 3.4: sample of Stainless steel316&430 with clamping device and standard tensile specimen

AISI 316 Stainless steel and AISI 430 Stainless steel plates with the dimensions of 100x85x3mm are rejoined together with the square butt weld design. Weld design is shown in Fig.3.1. MIG welding process was used using consumable electrode ER304 with diameter 1.2 mm. In each placement, distance between the nozzle and workpiece and the electrode extension were 20 and 10 millimeter, respectively. The welding electrode is held perpendicular to the welding surface. Welding is started and the flow rate of shielding gas is adjusted by using knob. The plates were welded at single pass.

The samples were tackwelded at either end so that a 1mm gap was left at the bottom of the plates. The shielding gas used was pure carbon dioxide with flow rate 10L/min. A set of preliminary trials were performed in order to optimize the experimental welding parameter and ensure good weld quality. Used welding condition and process parameters are given in Table 3.1.

3.2 Sample preparation for microstructure study and FESEM

After welding of both the specimen together with the MIG welding, a 20*10*3 mm section of the combination was cut using WIRE EDM machine. The part was cut in such a way that it includes the base metals of both the type, heat affected zone and the weld pool. Weld metal zone is the part melted during welding and retained in the weld. HAZ is the part of the parent metal that was not melted but metallurgically affected by the welding heat. These specimens were polished using emery paper of 1000 meshes. The final polishing was done by cloth polishing in the disc polishing machine using alumina powder. The specimens were etched by using a etchant which comprised a mixture of 30ml concentrated HNO₃, 30ml concentrated HCl and 30ml concentrated CH₃COOH in the ratio 1:1:1, applied

for 30 sec. Microstructural changes in the weldments were studied and recorded by optical microscope incorporated with image analysing software.



Fig.3.3: Prepared mould to use for microstructure study



Fig.3.5: Standard tensile specimen

3.3 Sample preparation for tensile test

The welded joints of ASS 316 FSS 430 were cut using WIRE EDM machine to the required dimension for preparing tensile test specimen. The specimens were prepared according to the ASTM standard. Dimension of standard tensile specimen is shown in Fig 3.4 and 3.5.

IV. RESULT AND DISCUSSION

The testing operations were carried out on all the prepared samples and results were recorded for analysis. The values of metal deposition rate(MDR), weld width, Heat Input, tensile strength, Percentage elongation, temperature profile for welded section, heat affected zone, microstructure with respect to the corresponding input process parameter settings were calculated. The influence of different process parameters on the surface integrity are discussed in the succeeding sections.

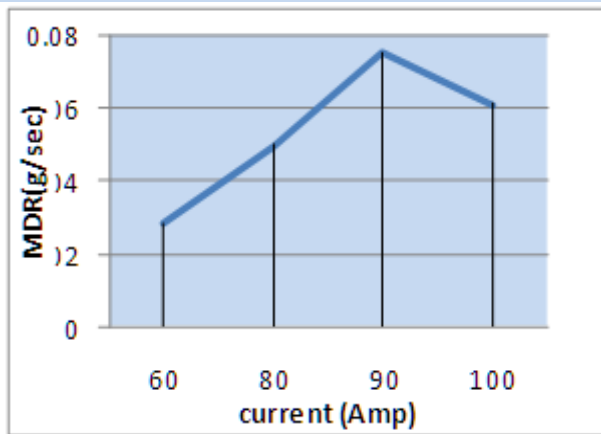
4.1. Metal Deposition Rate

The amount of welding material deposited per unit of time, expressed in gram per second is MDR. To calculate this we measure the weight of specimen before and after weld and the difference of this is divided by time which gives the MDR. The result shows in below table 4.1 and relation of all the results are shown in below graphs.

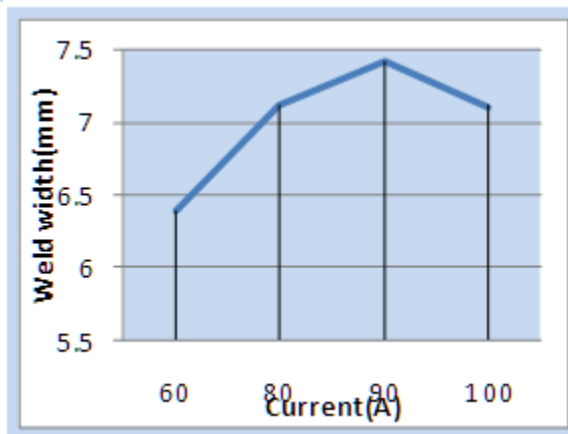
Table 4.1: Calculation of MDR and Weld width

| Job no. | Current (Amp) | Welding time (sec) | Weight before weld (g) | Weight after weld (g) | MDR (g/sec) | Weld width (mm) | Voltage (V)(vol) | Speed(S) (mm/s) | Heat Input = $(V \cdot I) / S$ (J/s) | Tensile Strength (MPa) |
|---------|---------------|--------------------|------------------------|-----------------------|-------------|-----------------|------------------|-----------------|--------------------------------------|------------------------|
| 1. | 60 | 50 | 301.25 | 302.68 | 0.0286 | 6.39 | 20 | 1.7 | 706 | 288.88 |
| 2. | 80 | 50 | 300.76 | 303.26 | 0.050 | 7.12 | 25 | 1.7 | 1176.47 | 311.12 |
| 3. | 90 | 50 | 301.11 | 304.87 | 0.0754 | 7.42 | 30 | 1.7 | 1588.24 | 333.28 |
| 4. | 100 | 50 | 302.20 | 305.26 | 0.0612 | 7.11 | 30 | 1.7 | 1764.7 | 328.88 |

The above result shows the effect of current on metal deposition rate and on the weld width. At low and moderate current MDR and weld width increases but at high temperature the MDR and weld width both decreases. This result is plotted in below graphs 4.1 and 4.2



Graph 4.1:MDRvs. Current



Graph 4.2:Weld Width vs. Current

4.2. Heat Input And Tensile Test

The tensile testing machine used has a maximum load capacity of 50 KN and operating with a cross-head speed of 5 mm/min. The jaws hold the tensile specimen from both extreme ends and starts pulling i.e. exerting tensile force. To hold the specimen with these jaws in easy manner it is required to make the specimen of I-section.

The computer connected to the tensile machine shows the following curve between the force and extensions as shown in graph 4.3 and 4.4. Each sample was tested accordingly in the testing machine and the corresponding curve between force and extensions was obtained. Here the force vs. extensions curves of sample 1 (which is welded with current 60 amp.) and 2 (which is welded with current 80 amp.) are shown below. From these curves the values of maximum forces are obtained. Then the initial area at the maximum force is calculated for the respective samples. The forces obtained were divided by these areas to obtain the ultimate tensile strength of the respective samples.



Graph 4.3: Force vs. Extension curve for Sample 1

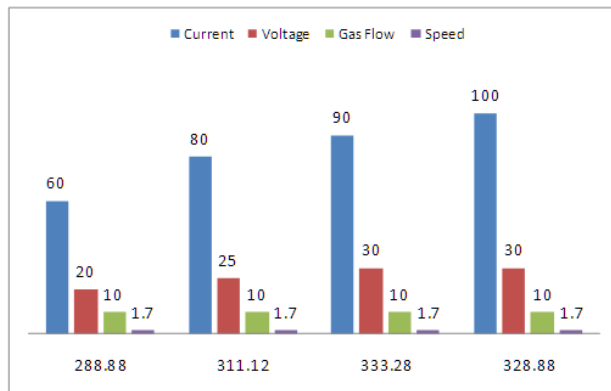


Graph 4.4: Force vs. Extension curve for Sample 2

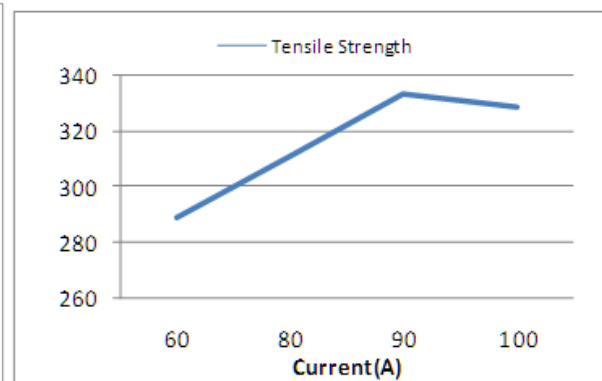
The tensile strength (TS) of base metal SS316 is 515MPa and for SS430 is 483MPa. Testing results of welded sample has maximum failure strength of 333.33MPa at 90 Amp and has minimum failure strength of 288.88MPa at

60 Amp current as shown in table 4.3. It can be seen from the above tables that as the values of current increases from 60 Ampere to 90 Ampere, the values of the tensile strength of the weldments increases from 288.88MPa(for sample 1 which is welded at 60 Amp) to 333.28MPa(for sample 3 which is welded at 90 Amp). Further it can be seen that the value of tensile strength for sample 4 (which is welded at 100 Amp) decreases as the current value further increases to 100 Ampere. This happens perhaps because as the current value increases,more heat is generated at the weld zone which resulted in slow cooling rate and development of columnar and coarser grains at the weld zone and the HAZ respectively. As the grains becomes coarse, brittleness of material increased and thus the tensile strength decreased.

When the welding current is too small, the root of the welded joint can be unwelded, this lead to the low tensile strength welded joint. When the welding current is too high defect like undercutting and collapse appear in the layer. With the increment of welding current, the tensile strength of the welded joints go up first and then fall down.



Graph 4.5: Tensile Strength vs. Various Parameters



Graph 4.6: Tensile Strength vs. Current

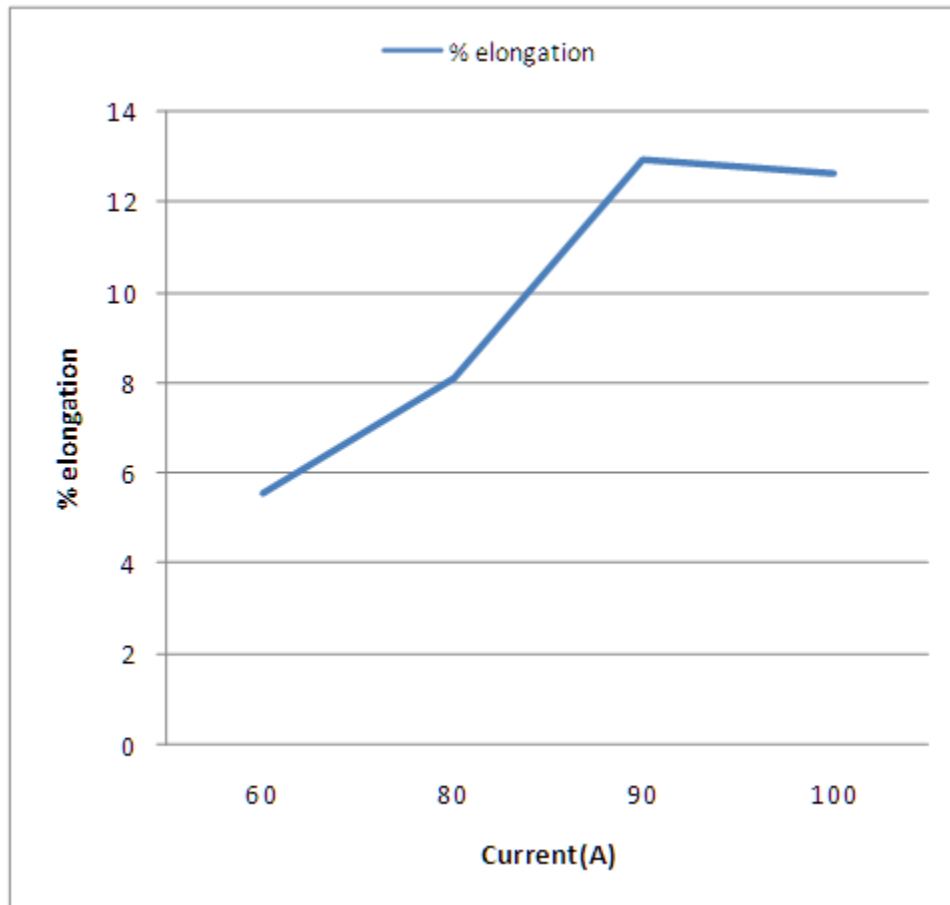
4.3. Percentage(%) Elongation

In the tensile testing machine, the specimens were gripped from both the ends. The distance between the grips is the Gauge length which is 65 mm. As the tensile testing machine started pulling i.e. exerted tensile force, the extensions of the specimen occurs. The values for the extensions of the various samples were calculated by subtracting the final length obtained after breaking and the gauge length as shown in table 4.4. The minimum extension was obtained for the sample 1 which was welded at 60 Ampere,20 volt and the maximum extension was obtained for the sample 3 which was welded at 90 Ampere, 30 volt.

Table 4.4: Percentage Elongation of Weldments for Austenitic Stainless Steel and Ferritic Stainless Steel

| SL.No. | Original Gauge Length (mm) (B) | Length after Breaking (mm)(A) | Difference(C)= (A-B)(mm) | %elongation |
|--------|--------------------------------|-------------------------------|--------------------------|-------------|
| 1 | 65 | 78.60 | 3.6 | 5.54 |
| 2 | 65 | 80.25 | 5.25 | 8.08 |
| 3 | 65 | 83.40 | 8.4 | 12.92 |
| 4 | 65 | 83.20 | 8.2 | 12.62 |

Graph 4.7: % elongation vs. Current



It can be concluded from the above data that the extension values increases as the current increases upto certain value of current. But extension value decreases as the current reaches 100 Ampere. This happens perhaps because as the current value increases, Tensile Strength increases and thus the extension of gauge length increases. Further, with increase in current value large fusion of base metals and filler metal takes place. But this happens upto certain value of current. Again increasing current beyond this certain limit(which is 90 Amp) to 100 Ampere , the tensile strength decreases and thus the extension decreases and the specimen breaks. The graph between percentage elongation and current is shown below in graph 4.7

V. TEMPERATURE PROFILE OF WELDZONE

The infrared camera clearly reveals the temperature profile at currents 60,80,90 and 100 Ampere. From the temperature profile we can see that at 60 Ampere current, the maximum temperature is 841.4⁰c. Similarly the maximum temperature for the sample 2, 3,4 (which are welded at 80,90 and 100 Ampere currents respectively) are 1345.8 ⁰c, 1640.9 ⁰c and >2000 ⁰c respectively. The figures related to the above said conditions are clearly shown below.

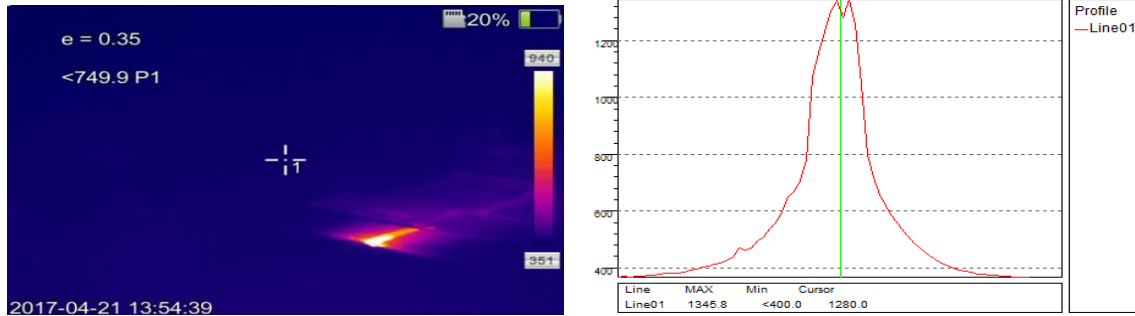


Fig 4.1: Temperature profile at current 60 ampere

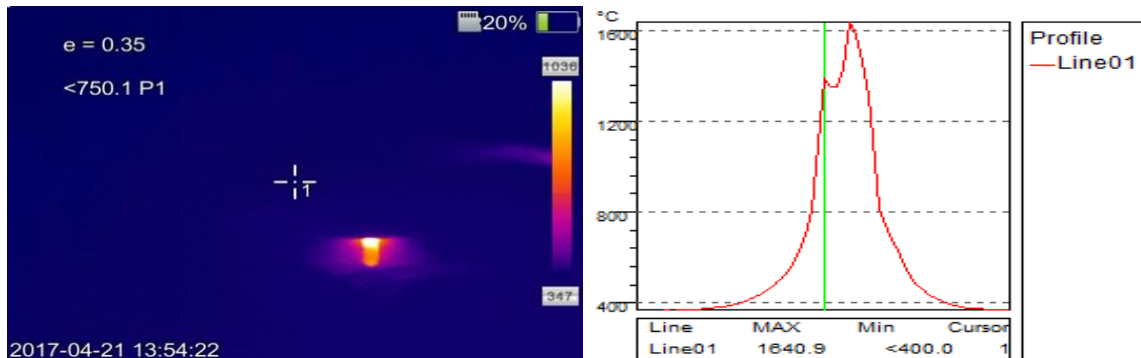


Fig 4.2: Temperature profile at current 80 ampere

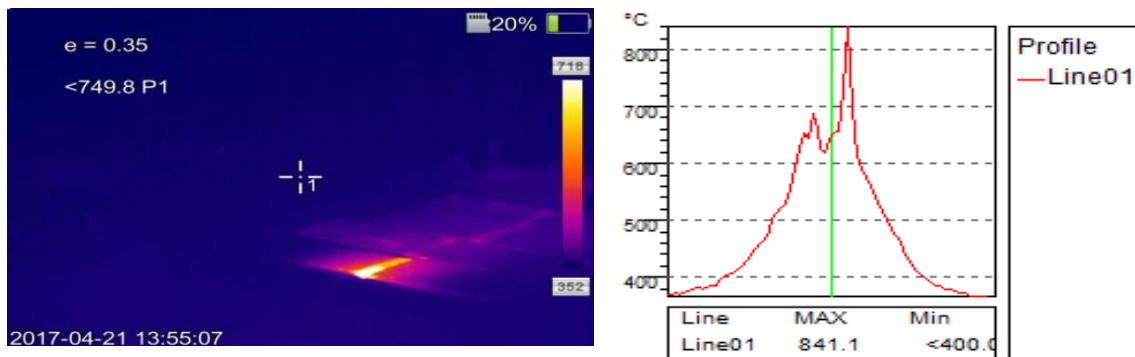


Fig 4.3: Temperature profile at current 90 ampere

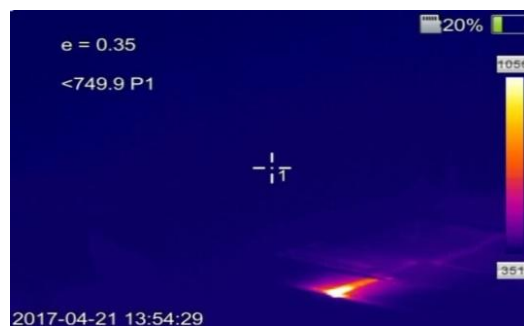


Fig 4.4: Temperature profile at current 100 ampere

VI. METALLOGRAPHY

The images of the welded sample at different processing condition were taken at Olympus microscope at IIT(ISM), Dhanbad for the study of weld bead geometry. Images of microstructure of welded sample is shown in figure (4.6-4.8). The figure clearly shows a grain growth occurs in welded and HAZ zone. Three zones properly fuses and HAZ appears near the welding zone or fusion zone.



Fig 4.5: Grain structure of Base metal of SS430 and SS316

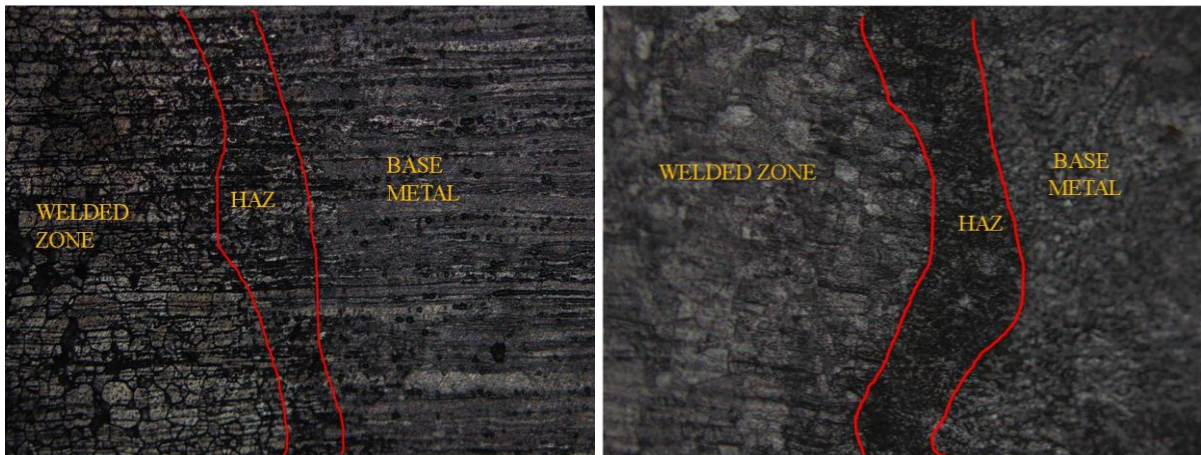


Fig 4.6: Grain structure of Dissimilar Welded SS316 & SS430 at 80, 90 and 100 Amp

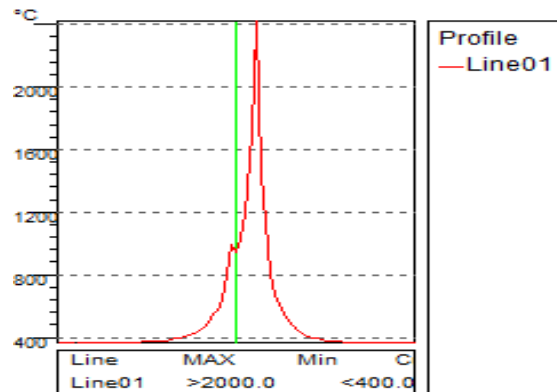


Fig.4.7: Fusion of Filler Wire & Base Metal SS 316

From the above figure we can conclude that by increasing the welding current the HAZ value increases and the grain growth is more at high current which is shown in figure 4.6. and 4.7. Also at weld zone columnar grain appears and at HAZ we get coarse grain structure.



Fig.4.8: Grain growth after Re-crystallization of weld zone

6.1 Microstructures by FESEM

The characterization of the material was done using its microstructure analysis and comparing the microstructures of the material in the welded zone with the base metal zone. The images of the microstructures were taken up to 1.0KX magnification using field effect scanning electron microscope (FESEM). The specimens were etched using a solution of hydrochloric acid (33 parts), nitric acid (33 parts), and Acetic acid (33 parts) to reveal the microstructure. The specimens were poured inside the reagent for three minutes. At last the images were taken with the help of field effect scanning electron microscope (FESEM).

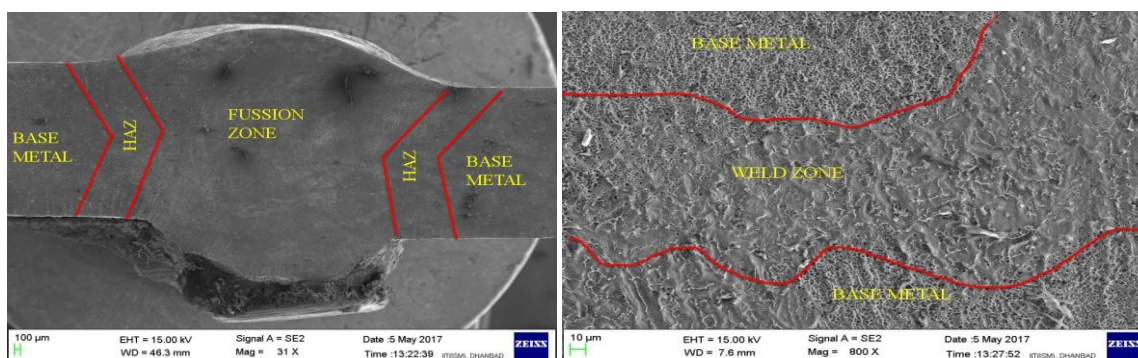


Fig.4.8: FESEM image of base metal, HAZ and Fusion zone at 90 Amp

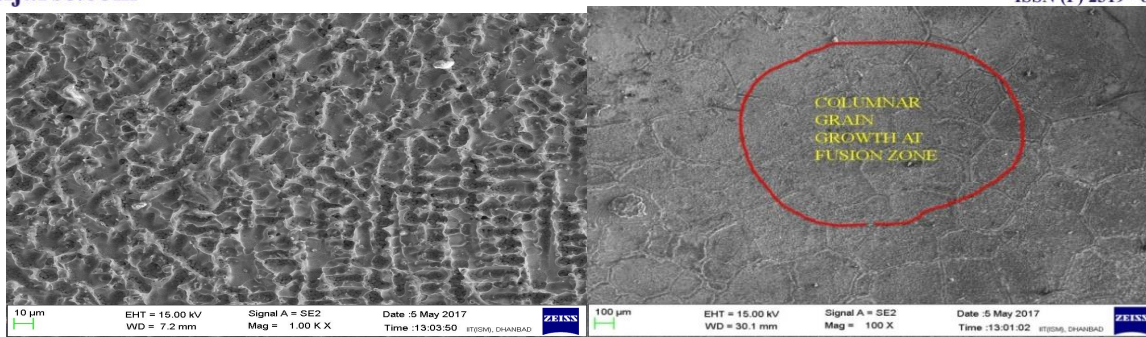


Fig.4.9:(a) Dendritic structure (b) Columnar grain

VII. CONCLUSION

With the automated welding system uniform welding of stainless steel plate can be possible. Based on the experimental results obtained from the different welding conditions, the following conclusions may be drawn.

- a.) Metal deposition rate (MDR) increases at low and moderate current but decreases as the current value increases further.
- b.) Weld width of the weld joint increases with increase in current.
- c.) Welding strength or tensile strength of the weld joint depends on the welding parameters like welding current and number of pass.
- d.) Tensile strength of the weldments increases as the current increases up to an optimum value but decreases as the current is increased further.
- e.) With increase in current more heat is produced at the weldment. More heat at weldment makes it brittle which decreases the tensile strength.
- f.) With DCEP, more heat is generated at workpiece resulting more penetration, wider weld width and higher tensile strength.
- g.) Optical microscopy result shows at Low current less HAZ but at high current it is more.
- h.) Percentage elongation of gauge length increases as the current is increased upto a certain value of optimum current but decreases further as the current is increased.
- i.) Temperature of weld zone is maximum. As current increases temperature at the weld zone increases.

VIII. FUTURE SCOPE

The effect of process parameters on MIG welding of SS316 & SS430 sheets of thickness 3mm has extensively been investigated in the present study. In many applications, a larger thickness is used and the present investigation may provide an insight for the MIG welding of dissimilar thicker stainless steel sheets. MIG welding of dissimilar materials is a recent (relatively) approach in the field of welding research. This should be exploited. Explanation of results obtained in the present study is one limitation of the present study. The results should be validated through proper mathematical modeling.



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